

Banja Luka 03.03.2020

Knowledge FOr Resilient soCiEty KURS CJELOŽIVOTNOG UČENJA PROTIVPOŽARNE GRAĐEVINSKE MJERE

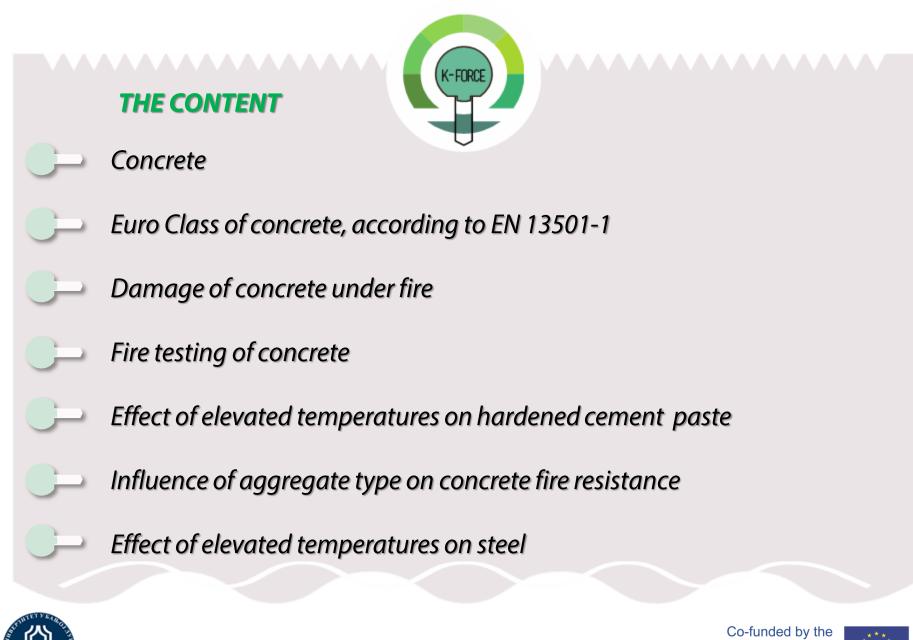
SVOJSTVA BETONA U USLOVIMA POŽARA Doc. Dr Gordana Broćeta



Co-funded by the Erasmus+ Programme of the European Union



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CONCRETE

















According to the decision of the European Commission (94/611/EC), which was published in the official journal of the European Community No. L 241/25, according to EN 13501-1, the **concrete** is classified as

Euro Class A1,

which does not require a fire resistance testing.





It is assumed that such a **concrete consists of:**



natural aggregates, conforming to EN 12620 for normal-weight aggregates and heavy-weight aggregates and EN 13055-1 for light-weight aggregates, cement, conforming to EN 197-1, water, conforming to EN 1008, admixtures, conforming to EN 934-2, additions, conforming to EN 12620 for powder aggregates, pigments, conforming to EN 12878, fly ash, conforming to EN 450, silica fumes, conforming to EN 13263 or other inorganic component materials, conforming to EN 206.





REACTION TO FIRE

Classification according to EN 13501-1

The aim of EN 13501-1 is to define procedure for the classification of **reaction to fire** of construction products.

It applies to three categories, which are treated separately - construction products, floorings and linear pipe thermal insulation products.

Definition	Construction products				Floorings		
	A1				A1 ₈		
non-combustile materials	A2 - s1 d0 A2 - s2 d0 A2 - s3 d0	A2 - s1 d A2 - s2 d A2 - s3 d	11	A2 - s1 d2 A2 - s2 d2 A2 - s3 d2	A2 ₈ - s1	A2 _# -s2	
combustible materials - very limited contribution to fire	B - s1 d0 B - s2 d0 B - s3 d0	B - s1 d B - s2 d B - s3 d	1	B - s1 d2 B - s2 d2 B - s3 d2	B _{ff} - s 1	B _{ff} - s2	
combustible materials - limited contribution to fire	C - s1 d0 C - s2 d0 C - s3 d0	C - s1 d C - s2 d C - s3 d	1	C - s1 d2 C - s2 d2 C - s3 d2	C _H - s 1	C _H -sl	
combustible materials - medium contribution to fire	D - s1 d0 D - s2 d0 D - s3 d0	D - s1 d D - s2 d D - s3 d	1	D - s1 d2 D - s2 d2 D - s3 d2	D _{ff} - s 1	D _H -s1	
combustible materials - highly contribution to fire	E		E - d2		E _n		
combustible materials - easily flammable	F					F _R	

https://www.peroni.com/lang_UK/_download/EN_Reaction_to_Fire_Classification.pdf

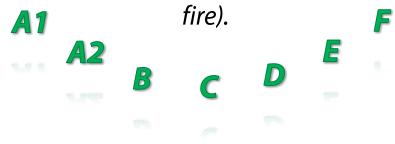




not be confused with



... is a response of a product in contributing by its own decomposition to a fire to which it is exposed, under specified conditions (means how the material itself reacts in the case of



... is the ability of building components and systems to perform their intended fire separating and/or loadbearing functions under fire exposure.

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FIRE RESISTANT





CONCRETE





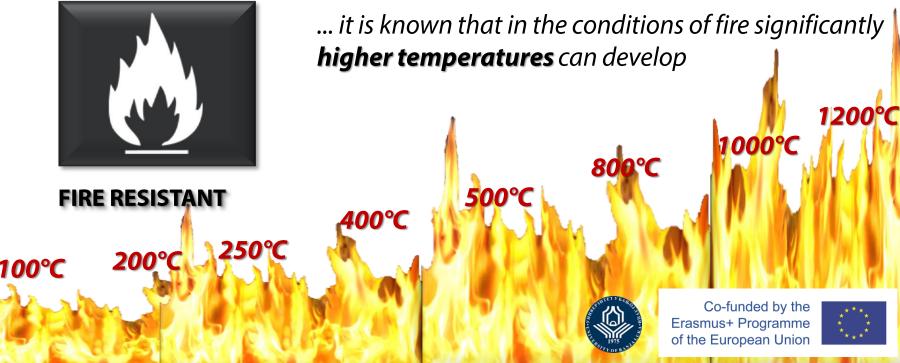


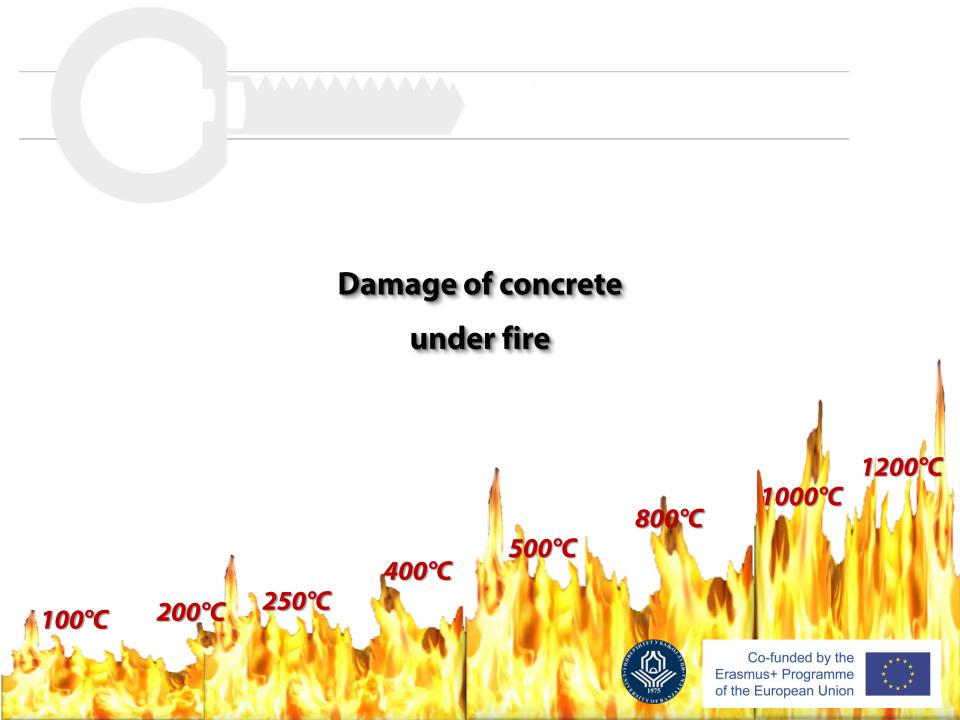




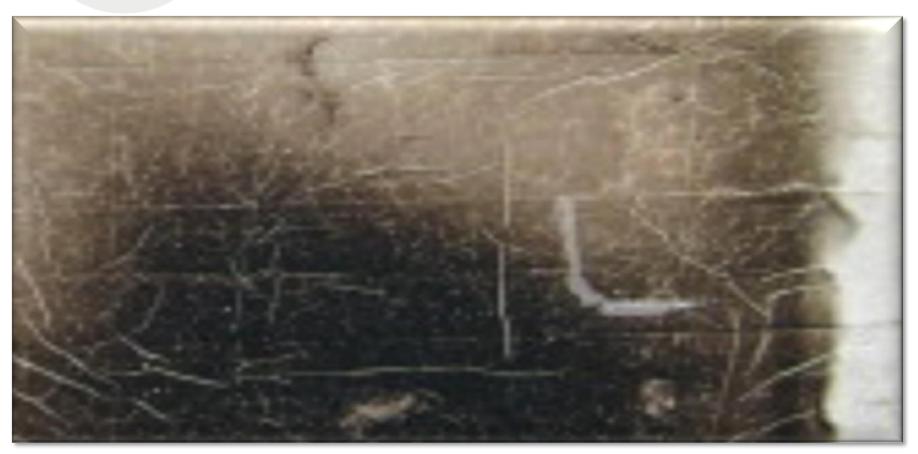
NOTE

the stated fire resistance refers to temperatures **up to 100°C**





Random hair cracks formed due to fire



https://www.researchgate.net/figure/Cracks-formed-due-to-fire_fig1_257681415





Concrete spalled from a slab soffit revealing pink/red discolouration



https://www.sandberg.co.uk/investigation-inspection/inspection/fire-damaged-concrete.html





Spalling of concrete to beams and a column caused by fire



https://www.sandberg.co.uk/investigation-inspection/inspection/fire-damaged-concrete.html





Reinforcement on a beam soffit exposed following a fire



https://www.sandberg.co.uk/investigation-inspection/inspection/fire-damaged-concrete.html



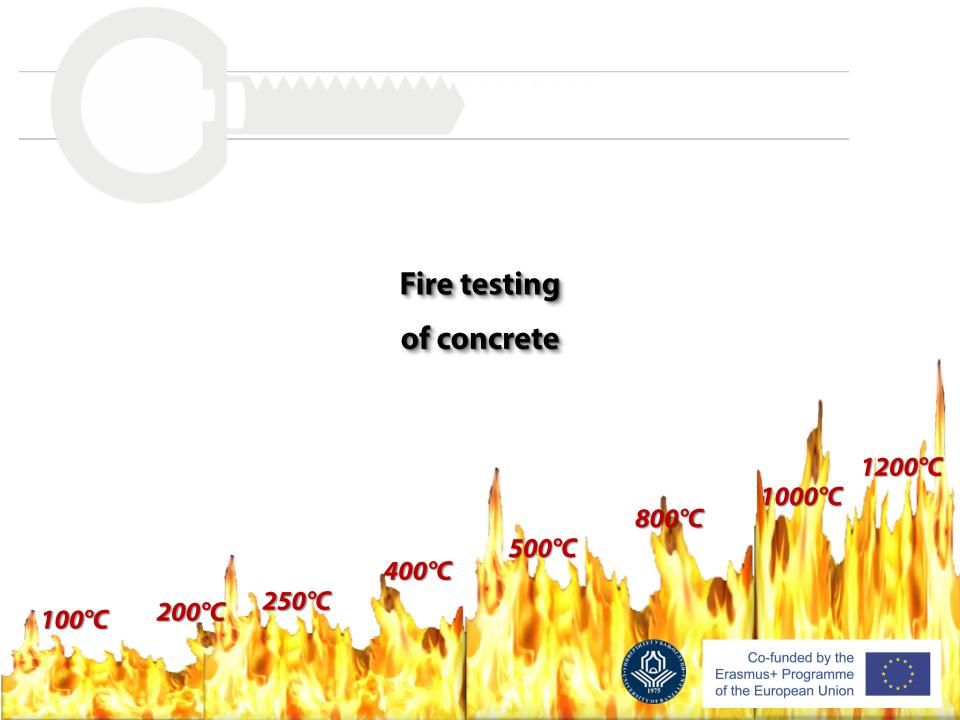


Colapse of floor construction exposed to fire



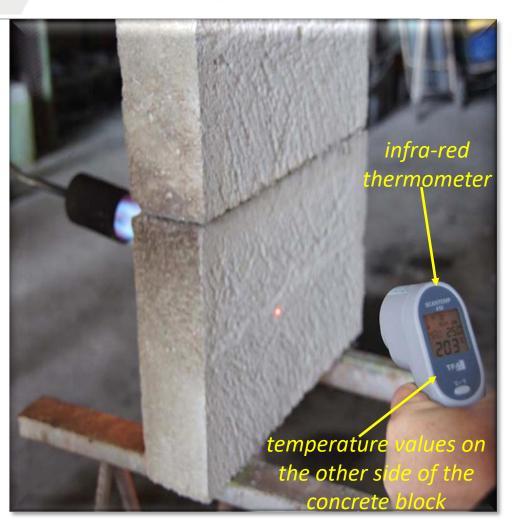








http://www.acimalta.eu/aciproperties.html





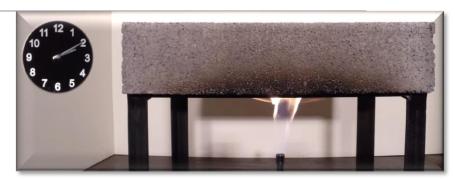


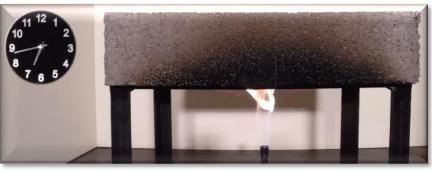
https://www.youtube.com/watch?v=_y m5x506B5A









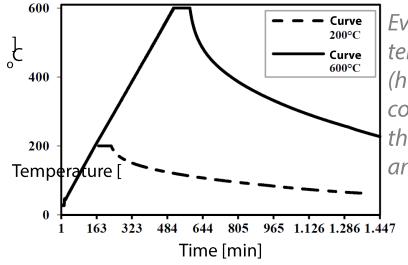








conforming to Recommendation of RILEM TC 200-HTC



Evolution of temperatures (heating and cooling mode for the oven, 200°C and 600°C)



Electric stove



Samples arranged in the stove

https://dr.nsk.hr/islandora/object/gfos:177/preview







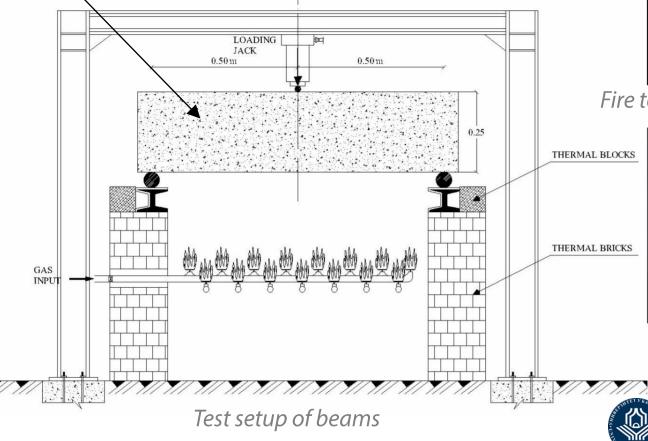
Co-funded by the Erasmus+ Programme of the European Union



The appearance of the samples after testing

Amr W. Sadek, M. El-Hawary, Amr S. El-Deeb: Fire Resistance Testing of Concrete Slabs Reinforced by GFRP Rebars, European Journal of Scientific Research, Vol.15 No.2 (2006), pp. 190-200 https://www.researchgate.net/publication/250146419_Fire_Resistance_Testing_of_Concrete_Slabs_Reinforced_by_GFRP_Rebars

Concrete slabs reinforced by glass fiber reinforced polymer rebars





Fire testing of beam specimen



Fire penetrating cracks in beam specimen





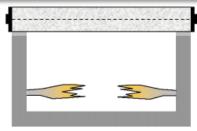


Fire testing of concrete

Concrete spalling during a fire test at Efectis Nederland

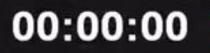
https://www.youtube.com/watch?v=CixMjo5VtgA

Time [min.]	Temperature [°C]		
0	20		
3	890		
5	1140		
10	1200		
30	1300		
60	1350		
90	1300		
120	1200		
>120	1200		

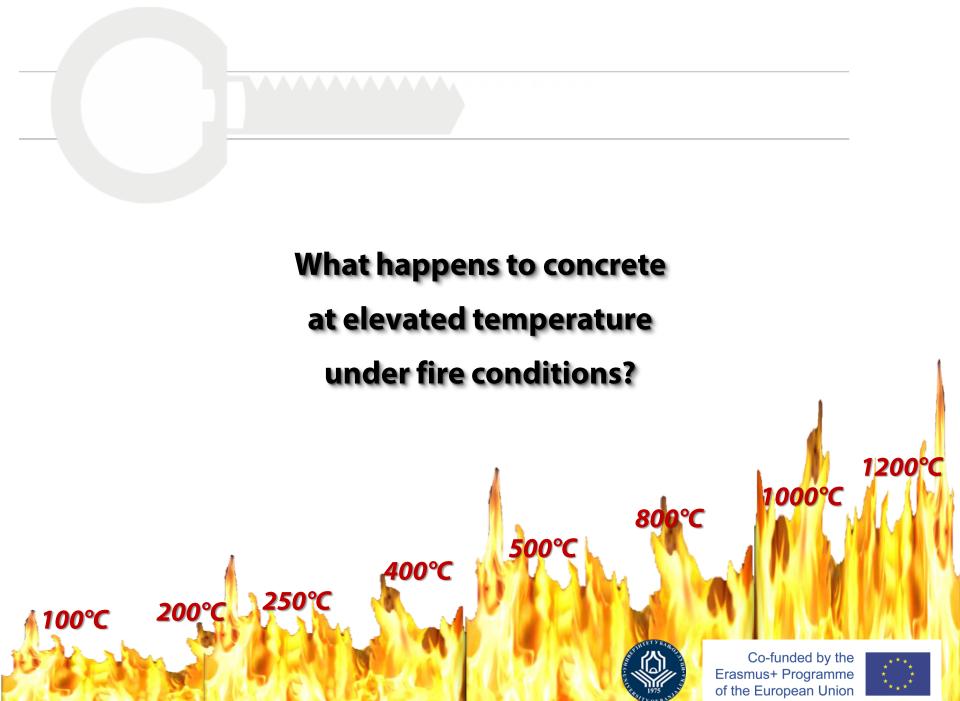




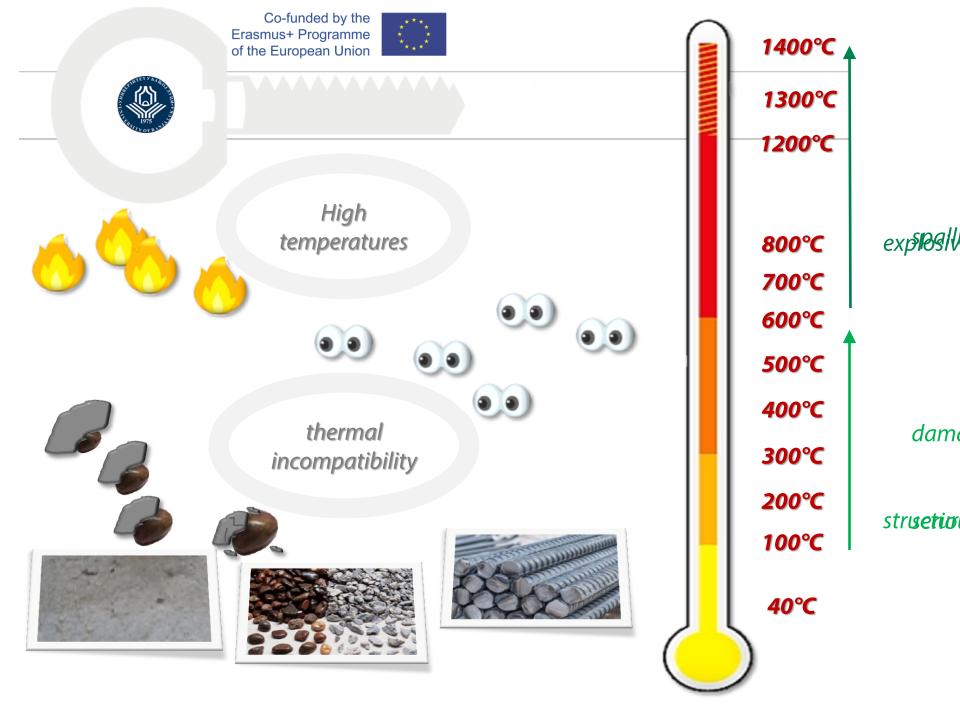


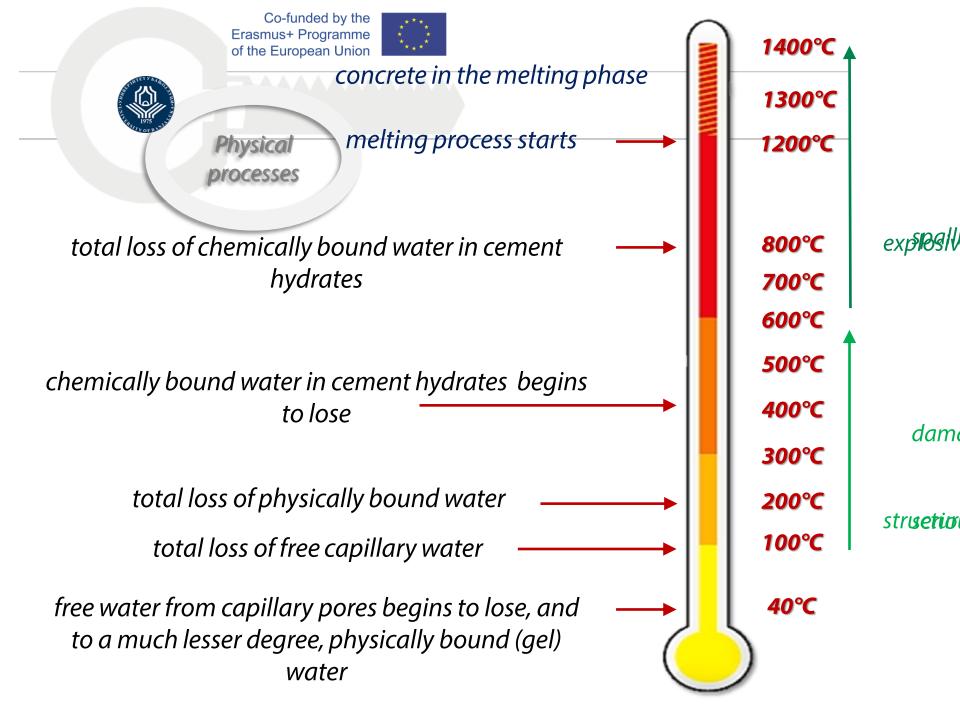






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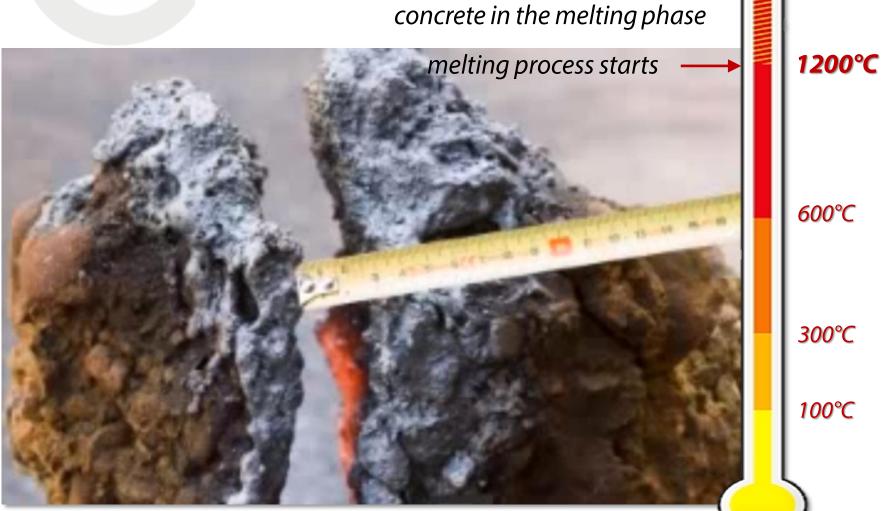








Molten decomposed concrete

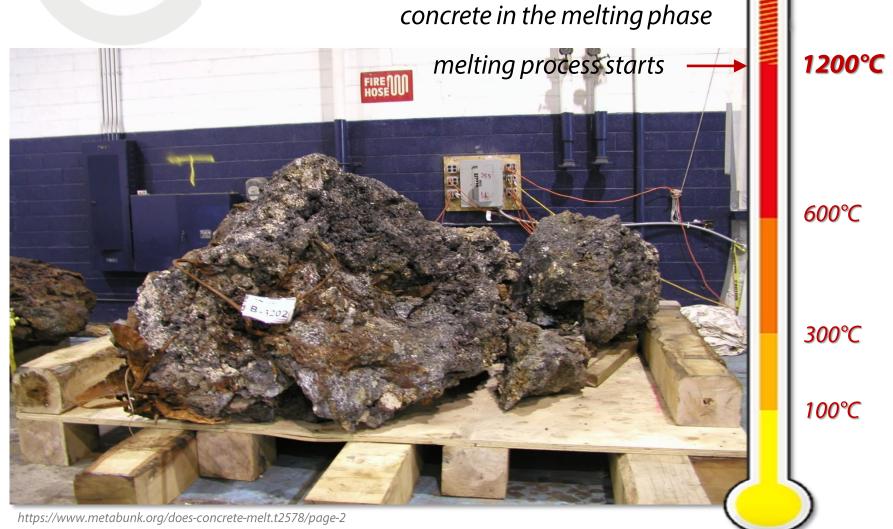


https://www.metabunk.org/does-concrete-melt.t2578/





Molten decomposed concrete







melting process starts

Chemical transformations

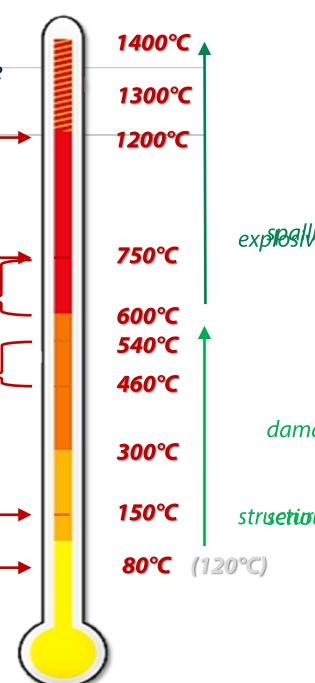
C-S-H gel has completely disappeared decomposition of the C-S-H (calcium-silicatehydrate phases) and formation of β-C₂S

> *decomposition of the portlandite (calcium hydroxide)*

 $Ca(OH)_2 \longrightarrow CaO + HO_2$

stability temperature of Tobermorite gel (C-S-H) C-S-H gel begins the process of dehydration

ettringite losses its crystalline form



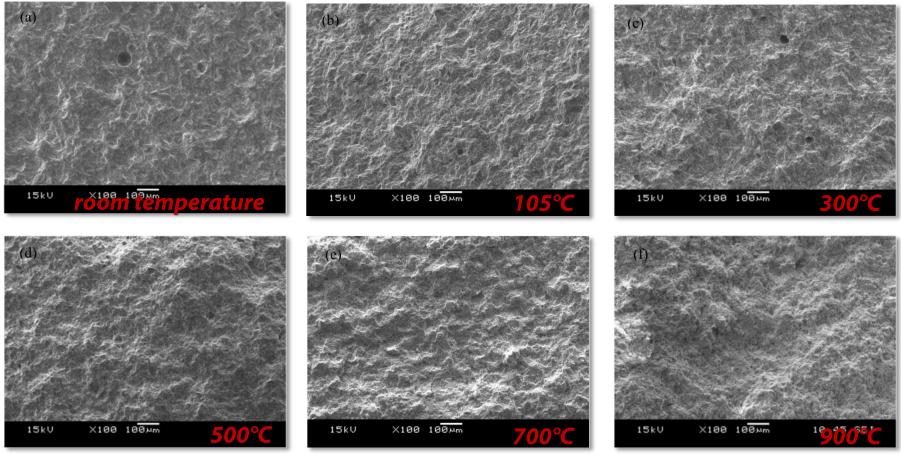




EXAMPLE OF RESEARCH

Seungmin Lim: Effects of elevated temperature exposure on cementbased composite materials, Dissertation, University of Illinois at Urbana-Champaign, 2015

SEM images of fractured surfaces of cement paste with w/c of 0.35 in 100× magnification





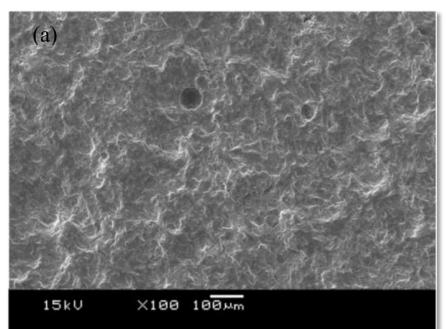


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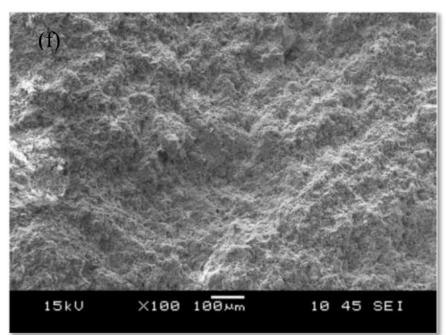
room temperature



surface roughness of a fractured surface increases as temperature increases

morphological changes as a function of exposure temperature

900°C



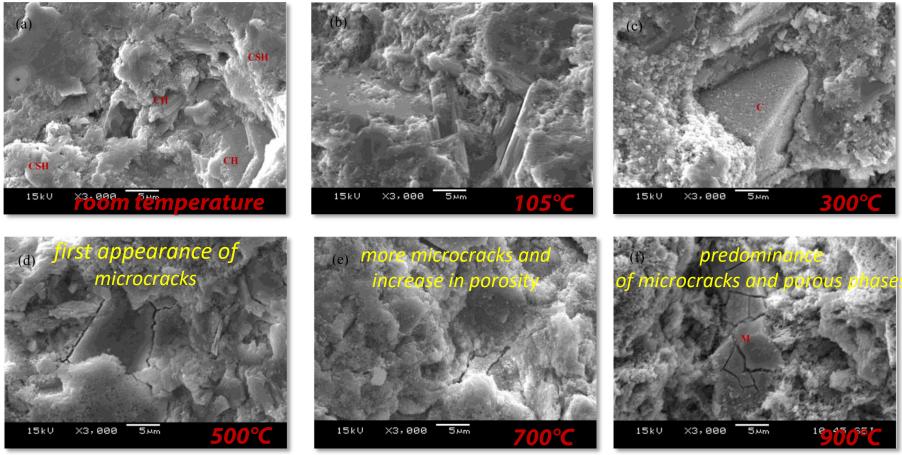




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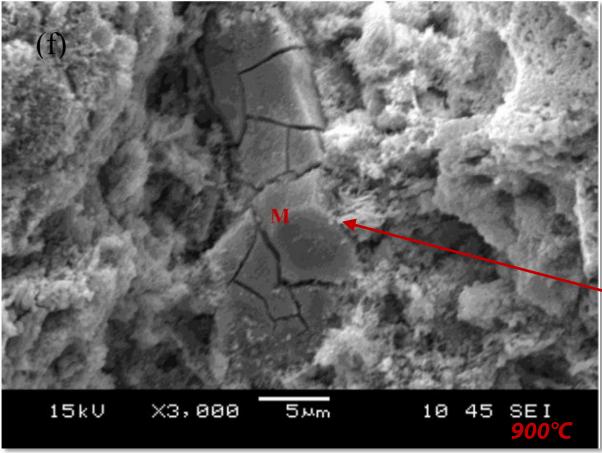
SEM images of fractured surfaces of cement paste with w/c of 0.35 in 3000× magnification







SEM images of fractured surfaces of cement paste with w/c of 0.35 in 3000× magnification



predominance of microcracks and porous phases

some particles (marked as **M**) are totally cracked

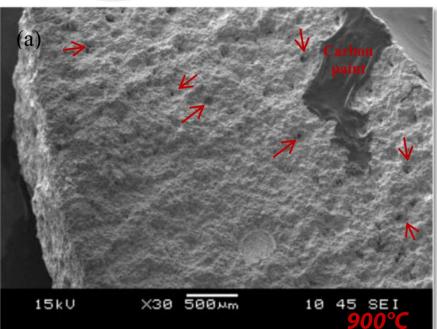




EXAMPLE OF RESEARCH

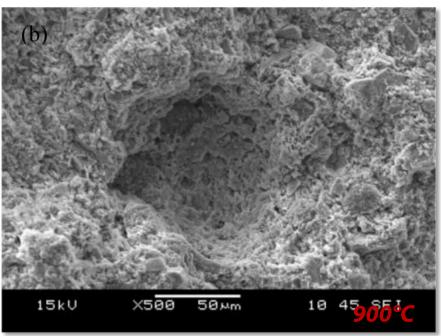
Seungmin Lim: Effects of elevated temperature exposure on cementbased composite materials, Dissertation, University of Illinois at Urbana-Champaign, 2015

SEM images of fractured surfaces of cement paste with w/c of 0.35 at 900°C in 30× and 500× magnifications



particles (possibly in unhydrated phases) *"popping out" of the paste* ... the exact cause of these voids could not be established

large spherical voids (approx. 50 μm) appear on areas of the fractured surface



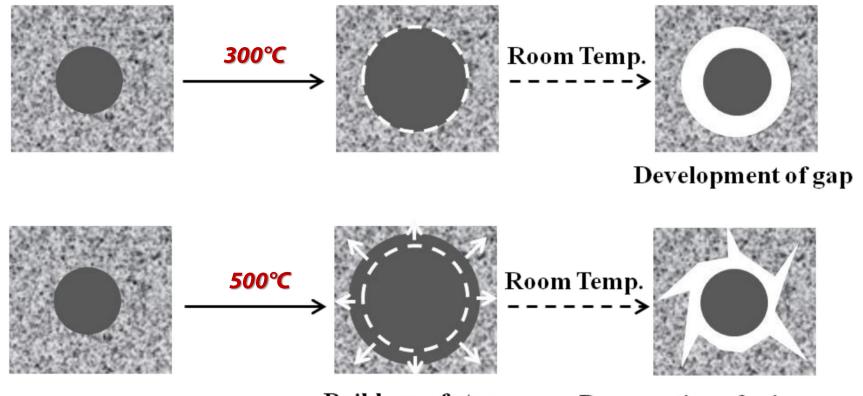




EXAMPLE OF RESEARCH

Seungmin Lim: Effects of elevated temperature exposure on cementbased composite materials, Dissertation, University of Illinois at Urbana-Champaign, 2015

Schematic diagrams of the formation of a gap a and propagation of microcracks at the interface between unhydrated cement particle and paste matrix



Build-up of stress

Propagation of micro-cracks



Influence of aggregate type on concrete fire resistance

Aggregates of metamorphic rocks

Ouartzite

Due to a significant content of quartz, which in conditions of intense heating is considered most critical mineral of solid rock, at elevated temperatures (over 500°C) they show signs of degradation - cracking.

50℃ increases volume by 0,17%

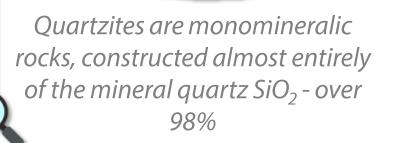
573℃ the largest expansion

polymorphic

transformation 🔰

http://www.quartzpage.de/gen_ro k.html

a quart $z \rightarrow$ high-temperature β quart z



the least favorable aggregates

Influence of aggregate type on concrete fire resistance

Aggregates of igneous rocks (granite, dacite, senitite, diorite, adensite, gabar, basalt, diabase)





are generally characterized by **good resistance** to the action of elevated temperatures, although they contain mineral quartz.

Diorite Star Adensite

Given the fine-grained structure with well distributed mineral content and proportionally relatively low content of quartz, this cumstance has no significant influence.





Influence of aggregate type on concrete fire resistance

Aggregates of sedimentary rocks

Dolomite



Dolomite aggregate for concrete



calcite (CaCO₃)

Limestone



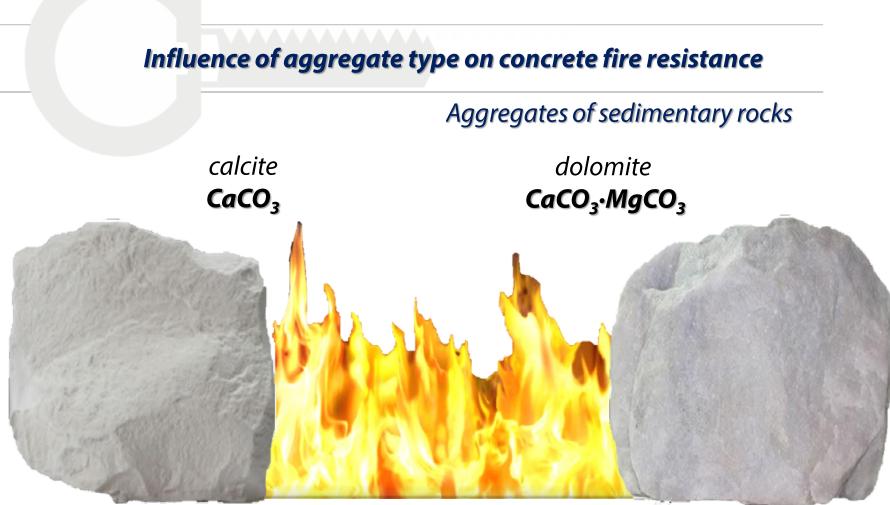


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dolomite

 $(CaCO_3 \cdot MgCO_3)$





Limestone

Dolomite





MgO



heating-up at a rate of 1°C/min

EXAMPLE OF RESEARCH

Zhi Xing, Ronan Hébert, Anne-Lise Beaucour, Béatrice Ledésert, Albert Noumowé: Influence of the nature of aggregates on the behaviour of concrete subjected to elevated temperature, Materials and Structures, November 2014, Volume 47, Issue 11, pp 1921–1940

Aggregates of sedimentary rocks (limestone aggregate)

< 600°C

600°C

no changes

color change for some particles of aggregates, becoming gradually more reddish

750℃

particles of aggregates are cracked and the particle surface has whitened





Decarbonation								
calcite	lime	carbon dioxide						
CaCO ₃ —	→ CaO +	CO ₂						

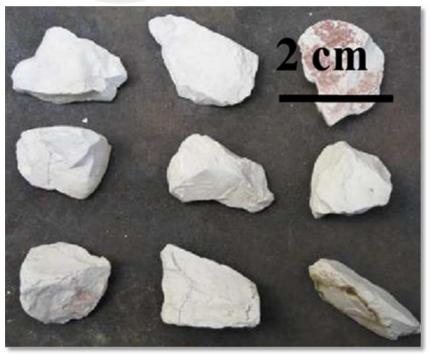


Appearance of the aggregate after heating at 750°C



Zhi Xing, Ronan Hébert, Anne-Lise Beaucour, Béatrice Ledésert, Albert Noumowé: Influence of the nature of aggregates on the behaviour of concrete subjected to elevated temperature, Materials and Structures, November 2014, Volume 47, Issue 11, pp 1921–1940

Aggregates of sedimentary rocks (limestone aggregate)





Appearance of the aggregateafter heating-cooling cycle at 750°C3 days after heating-cooling cycle

at 750°C



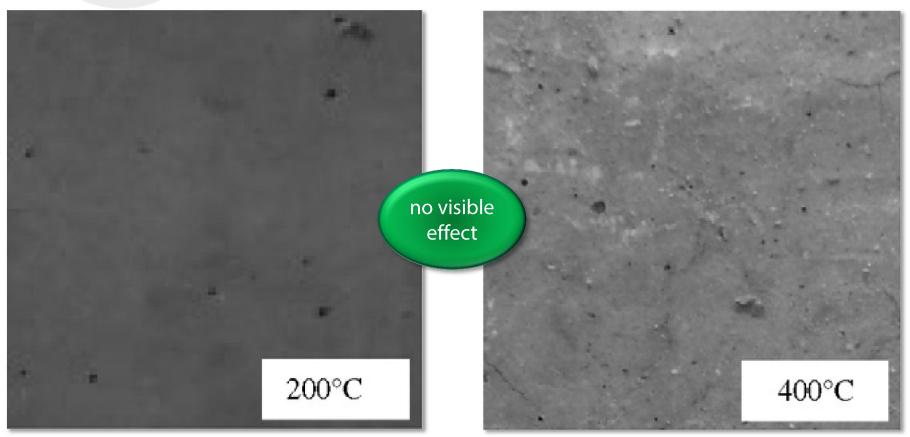
CaO

Ca(OH)₂ volume expansion of 200%



Omer Arioz: Effects of elevated temperatures on properties of concrete, Fire Safety Journal 42 (2007) pp. 516–522

Aggregates of sedimentary rocks (crushed limestone aggregate)



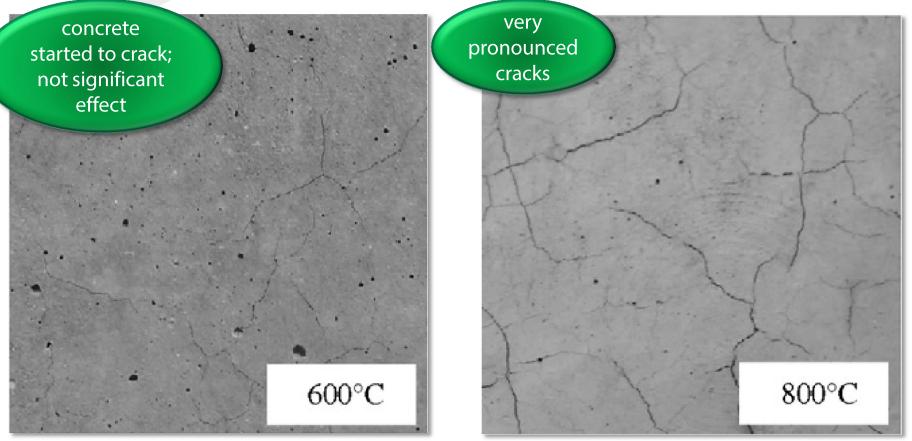
Surface texture of the concrete exposed to elevated temperatures





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Aggregates of sedimentary rocks (crushed limestone aggregate)



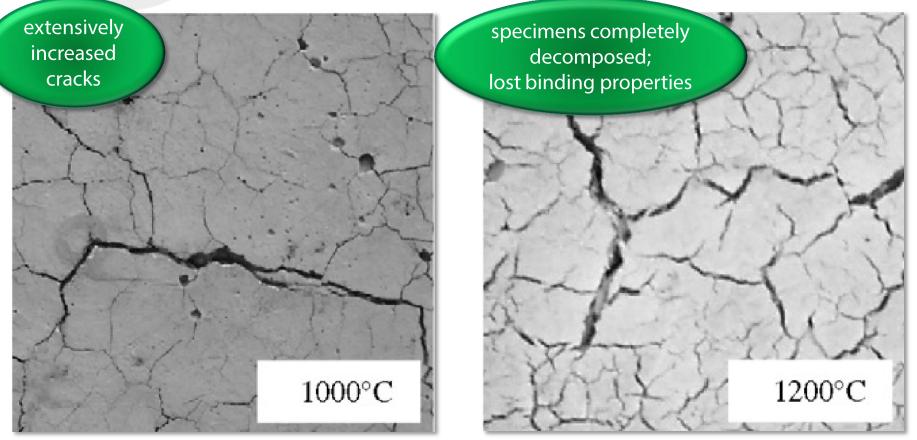
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Surface texture of the concrete exposed to elevated temperatures





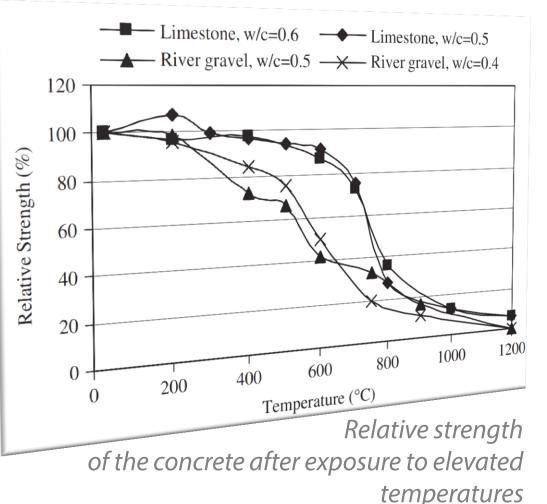




Omer Arioz: Effects of elevated temperatures on properties of concrete, Fire Safety Journal 42 (2007) pp. 516–522

Aggregates of sedimentary rocks (crushed limestone aggregate)

The effect of high temperatures on the relative strength of concrete was more pronounced for concrete mixtures produced by river gravel aggregate. This can be attributed to the siliceous composition of the river gravels.







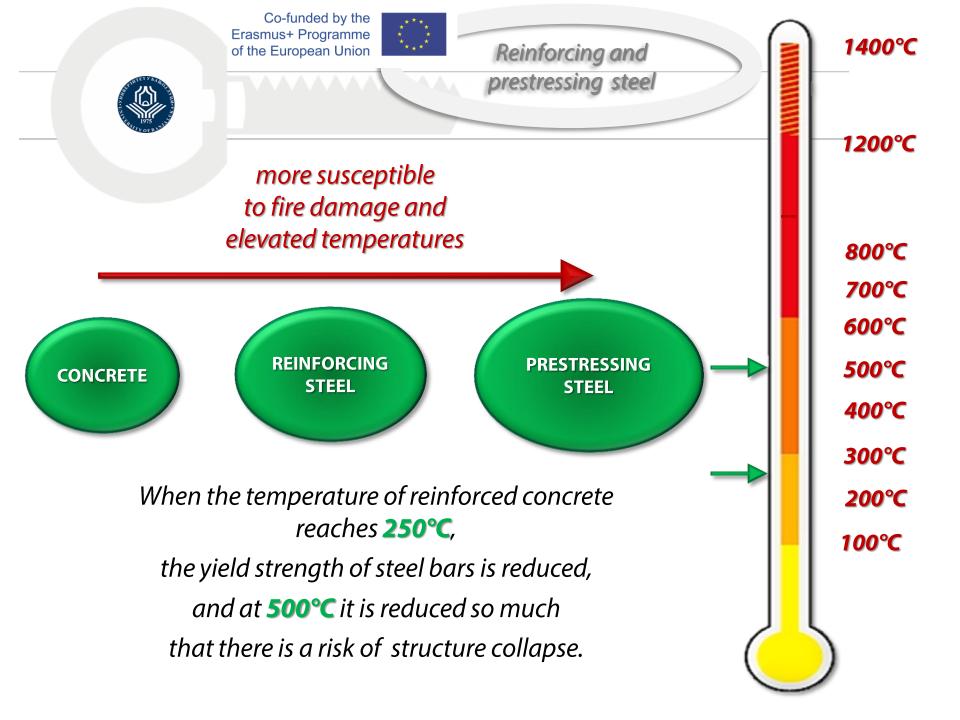


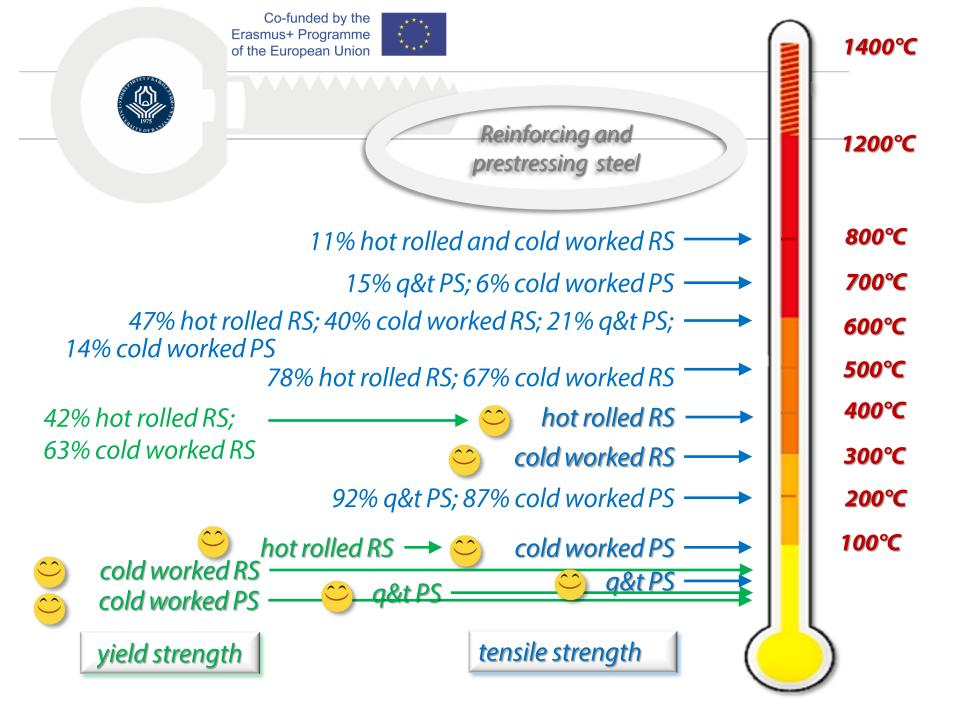
Values for the main parameters of the stress-strain relationships of **normal weight concrete**

Concrete

Concrete	Siliceous aggregates Calcareous aggregates		regates	with siliceous or calcareous							
temp. θ	$f_{c, \theta} / f_{ck}$	$\mathcal{E}_{c1,\theta}$	<i>E</i> _{cu1,θ}	$f_{c,\theta}/f_{ck}$	$\mathcal{E}_{c1,\theta}$	<i>E</i> cu1,θ	f				
[°C]	[-]	[-]	[-]	[-]	[-]	[-]	<i>ice</i> oggregates concrete				
1	2	3	4	5	6	7	at elevated				
20	1,00	0,0025	0,0200	1,00	0,0025	0,0200	temperatures				
100	1,00	0,0040	0,0225	1,00	0,0040	0,0225					
200	0,95	0,0055	0,0250	0,97	0,0055	0,0250					
300	0,85	0,0070	0,0275	0,91	0,0070	0,0275	$\varepsilon_{c1,0} \qquad \varepsilon_{cu1,0} \qquad \varepsilon_{cu1,0}$				
400	0,75	0,0100	0,0300	0,85	0,0100	0,0300	Coefficient $k_{c,t}(\theta)$ allowing for				
500	0,60	0,0150	0,0325	0,74	0,0150	0,0325	$\kappa_{s}(\theta)$ decrease of tensile strength ($f_{ck,t}$)				
600	0,45	0,0250	0,0350	0,60	0,0250	0,0350	1,0 of concrete at				
700	0,30	0,0250	0,0375	0,43	0,0250	0,0375	0,8 elevated				
800	0,15	0,0250	0,0400	0,27	0,0250	0,0400	0,6 temperatures				
900	0,08	0,0250	0,0425	0,15	0,0250	0,0425	0,4				
1000	0,04	0,0250	0,0450	0,06	0,0250	0,0450					
1100	0,01	0,0250	0,0475	0,02	0,0250	0,0475	0,2				
1200	0,00	-	-	0,00	-	-	0,0 0 100 200 300 400 500 600				
f_{ck} Characteristic compressive cylinder strength of concrete at 28 days θ [°C]											

 f_{ctk} Characteristic axial tensile strength of concrete











 $f_{sy,\theta}$

Esu,⊕ E

Values for the parameters of the stress-strain relationship of **hot rolled** and **cold worked RS** at elevated temperatures

Steel Temperature	f _{sy,}	_θ / f _{yk}	$f_{sp, heta}$	/ f _{yk}	$E_{s, heta}/E_s$		
θ[°C]	hot rolled	cold worked	hot rolled	cold worked	hot rolled	cold worked	
1	2	3	4	5	6	7	
20	1,00	1,00	1,00	1,00	1,00	1,00	
100	1,00	1,00	1,00	0,96	1,00	1,00	
200	1,00	1,00	0,81	0,92	0,90	0,87	
300	1,00	1,00	0,61	0,81	0,80	0,72	
400	1,00	0,94	0,42	0,63	0,70	0,56	
500	0,78	0,67	0,36	0,44	0,60	0,40	
600	0,47	0,40	0,18	0,26	0,31	0,24	
700	0,23	0,12	0,07	0,08	0,13	0,08	
800	0,11	0,11	0,05	0,06	0,09	0,06	
900	0,06	0,08	0,04	0,05	0,07	0,05	
1000	0,04	0,05	0,02	0,03	0,04	0,03	
1100	0,02	0,03	0,01	0,02	0,02	0,02	
1200	0,00	0,00	0,00	0,00	0,00	0,00	

 f_{yk} Characteristic yield strength of reinforcement

 $f_{sk}(\theta)$ Characteristic strength of reinforcing steel at temperature θ for a specified strain



Prestressing steel

EN 1992-1-2:2004

Values for the parameters of the stress-strain relationship of **cold worked (cw)** (wires and strands) and quenched and tempered (q&t) (bars) prestressing steel at elevated temperatures

Steel temp.	$f_{\mathrm{py}, heta}$ / (eta f_{pk})			$f_{ m pp, heta}$ / (eta f _{pk})		$E_{p, \theta} / E_{p}$		<i>Е</i> рt,θ [-]	<i>Є</i> ри,θ [-]
<i>θ</i> [°C]	C	w	q & t	CW	q&t	cw	q&t	cw, q&t	cw, q&t
	Class A	Class B							
1	2a	2b	3	4	5	6	7	8	9
20	1,00	1,00	1,00	1,00	1,00	1,00	1,00	0,050	0,100
100	1,00	0,99	0,98	0,68	0,77	0,98	0,76	0,050	0,100
200	0,87	0,87	0,92	0,51	0,62	0,95	0,61	0,050	0,100
300	0,70	0,72	0,86	0,32	0,58	0,88	0,52	0,055	0,105
400	0,50	0,46	0,69	0,13	0,52	0,81	0,41	0,060	0,110
500	0,30	0,22	0,26	0,07	0,14	0,54	0,20	0,065	0,115
600	0,14	0,10	0,21	0,05	0,11	0,41	0,15	0,070	0,120
700	0,06	0,08	0,15	0,03	0,09	0,10	0,10	0,075	0,125
800	0,04	0,05	0,09	0,02	0,06	0,07	0,06	0,080	0,130
900	0,02	0,03	0,04	0,01	0,03	0,03	0,03	0,085	0,135
1000	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,090	0,140
1100	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,095	0,145
1200	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,100	0,150
Note: For intermediate values of temperature, linear interpolation may be used.									

 f_{pk} Characteristic tensile strength of prestressing steel

 $f_{pk}^{(n)}(\theta)$ Characteristic strength of prestressing steel at temperature θ for a specified strain



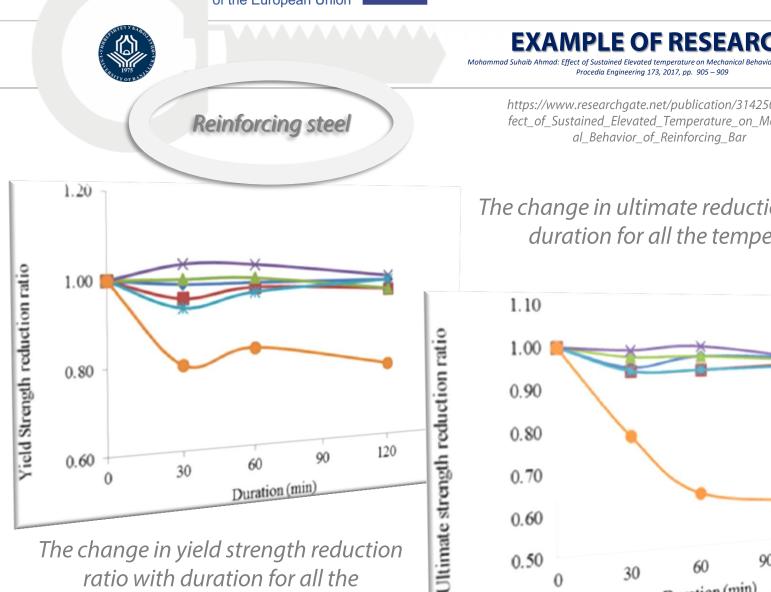


Mohammad Suhaib Ahmad: Effect of Sustained Elevated temperature on Mechanical Behavior of Reinforcing Bar, Procedia Engineering 173, 2017, pp. 905 – 909

Reinforcing steel 20 mm diameter bars were heated at temperatures 200, 300, 400, 500, 600 1.2 and 700°C and were sustained for 0.5,1 1 and 2 h. The bars were cooled naturally in air to 0.8 ambient temperature and were tested in Reduction ratio tension. 0.6 0.4 Reduction in yield strength vield strength Ultimate Strength is significantly higher 0.2 in comparison to 0 ultimate strength 200 400 600 800 0 Temperature in °C

Reduction ratio in yield strength and ultimate strength with increase in temperatures havior_of_Reinforcing_Bar





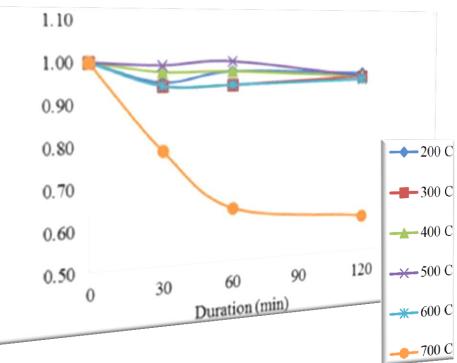
ratio with duration for all the temperature

EXAMPLE OF RESEARCH

Mohammad Suhaib Ahmad: Effect of Sustained Elevated temperature on Mechanical Behavior of Reinforcing Bar,

https://www.researchgate.net/publication/314250409 Ef fect_of_Sustained_Elevated_Temperature_on_Mechanic

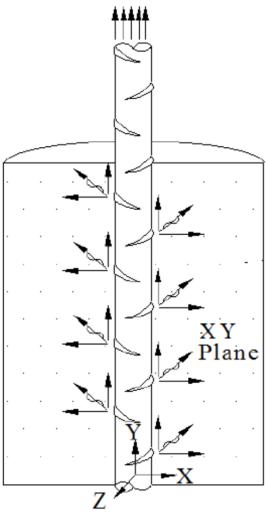
The change in ultimate reduction ratio with duration for all the temperatures





Bond between concrete and steel

The bond between concrete and steel can be adversely affected at temperatures higher than 300°C because of the greater thermal conductivity of steel compared to the cover concrete and differences in thermal expansion properties.



https://www.researchgate.net/publication/26614396 6_Bond_stress_behavior_between_concrete_and_ste el_rebar_Critical_investigation_of_pullout_test_via_Finite_Element_Modeling

Conclusion

CONCRETE

- There are differences in the meaning of the terms REACTION TO FIRE and RESISTANCE TO FIRE.
- According to EN 13501-1, the concrete is classified as Euro Class A1, which does not require a fire testing.
- **Type and properties of aggregate** play an important role on the properties of concrete exposed to elevated temperatures.
- *From the aspect of resistance to fire, the least favorable aggregates are obtained from rocks of metamorphic origin, primarily of quartzite rocks.*
- In this sense, dolomite aggregates, limestone aggregates, recycled aggregate of crushed brick and granulated slag, may be preferred.





Conclusion

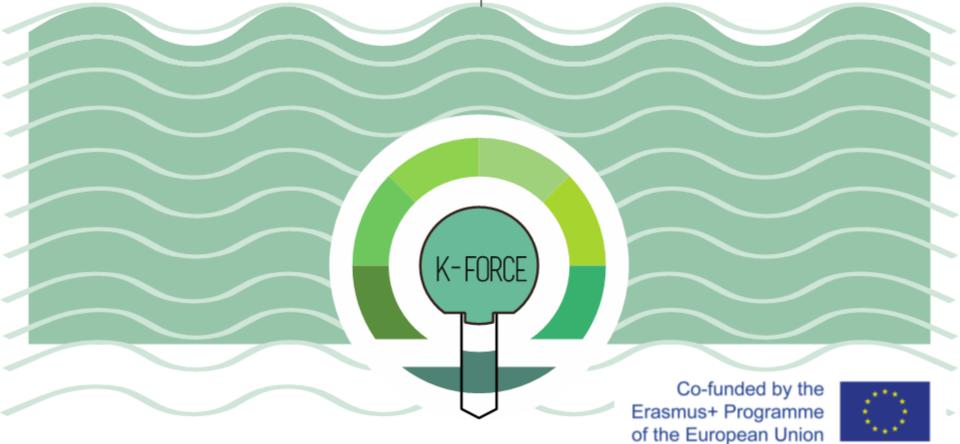
Steel is more susceptible to fire damage and elevated temperatures, compared to concrete.

- *Prestressing steel is more susceptible* to fire damage and elevated temperatures, compared to reinforcing steel.
- When the temperature of reinforced concrete reaches 250°C, the yield strength of steel bars is reduced and at 500°C it is reduced so much that there is a risk of structure collapse.
- *Reduction in yield strength is significantly higher in comparison to ultimate strength.*
- The bond between steel and concrete can be adversely affected at temperatures higher than 300°C.





STEEL



Thank you for your attention

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Knowledge FOr Resilient soCiEty